

MODELING THE PHASE DIAGRAM OF THE Tl₉GdTe₆ -Tl₄PbTe₃ -Tl₉BiTe₆ SYSTEM

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Abstract. The analytical multi-3D model of the phase diagram of the Tl₉GdTe₆-Tl₈Pb₂Te₆-Tl₉BiTe₆ system was obtained and visualized for the quasi-ternary and non-quasi-ternary high-temperature part. The analytical models of phase diagrams of the Tl₉GdTe₆ -Tl₈Pb₂Te₆ and Tl₉GdTe₆ -Tl₉BiTe₆ systems were obtained in the "temperature – composition" coordinates. The boundaries of the liquidus and solidus surface of crystallization of solid solutions and the TlGdTe₂ compound were obtained. The thermodynamic functions of mixing solid solutions were determined based on the model of regular solutions of non-molecular compounds. It was shown that solid solutions based on the ternary Tl₉GdTe₆, Tl₈Pb₂Te₆, and Tl₉BiTe₆ compounds have thermodynamic stability in the entire concentration range and the temperature range T = 300–780 K.

Keywords: Phase diagram, thallium-gadolinium tellurides, thallium-lead tellurides, thallium-bismuth tellurides, 3D modeling.

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1. Introduction

Chalcogenide rare-earth elements (REE) were studied for a long time due to their interesting physical properties such as superconductivity (Jha, 2014; Yarembash, 1975; Yumigeta *et al.*, 2021), mixed valences (Antonov, 2005), strong electron correlations (Kogar, 2020; Liu *et al.*, 2018), thermoelectric (Cheikh *et al.*, 2018; Wang *et al.*, 2011), magneto-optical properties (Yumigeta *et al.*, 2021; Boncher *et al.*, 2015; Guo, 2014; Verma, 2009; Xing *et al.*, 2020) et al. In particular, authors (Yumigeta *et al.*, 2021; Xing *et al.*, 2020) showed the promise for use of REE tritellurides in the high energy storage density, magnetic sensors, magnetic twistrionic devices, and spintronics.

Development of methods for directed synthesis of new materials based on REE chalcogenides is based on reliable data on phase equilibria and thermodynamic data of the corresponding systems (Babanly *et al.*, 2017, 2019; Imamaliyeva, 2018a).

Subtelluride Tl₅Te₃ which exhibits thermoelectric properties [Matsumoto *et al.*, 2009] due to the peculiarities of the crystal lattice, has many ternary analogs of the types Tl₉AX₆ and Tl₄BX₃ (A-Sb, Bi, In, Au, REE; B-Sn, Pb, Mo, Cu, rare-earth elements; X-Se, Te) (Imamaliyeva, 2018a, 2020a, b; Wacker, 1991; Doert, 1994; Bradmüller, 1993, 1994a,b; Piasecki *et al.*, 2017; Plucinski *et al.*, 2015), also possessing several functional properties, namely optical (Piasecki *et al.*, 2017; Plucinski *et al.*, 2015), thermoelectric (Khan *et al.*, 2020; Guo, 2015), magnetic (Bangarigadu-Sanasy *et al.*, 2014; Isayeva *et al.*, 2020), as well as topological insulators properties (Arpino *et al.*, 2015; Niu *et al.*,

2014). In recent years, to improve thermoelectric performance, intensive work has been carried out to study solid solutions and doped phases based on these compounds (Khan *et al.*, 2020; Guo *et al.*, 2014a).

To obtain new variable composition phases with Tl_5Te_3 -structure, we studied phase relations in some systems consisting of Tl_5Te_3 and its ternary analogs (Imamaliyeva *et al.*, 2018b; Babanly *et al.*, 2008; Imamaliyeva *et al.*, 2017a, b). It was obtained that studied systems are characterized by the formation of continuous series of solid solutions at the solidus temperatures and below, which are crystallized in the tetragonal Tl_5Te_3 structure type.

As a continuation of the studies of the listed systems, in (Imamaliyeva *et al.*, 2020c; Imamaliyeva *et al.*, 2021) the 3D modeling of the phase diagrams of the Tl_9SmTe_6 - Tl_4PbTe_3 - Tl_9BiTe_6 and Tl_9TbTe_6 - Tl_4PbTe_3 - Tl_9BiTe_6 systems was carried out.

The purpose of this article is 3D modeling of the phase diagram of the Tl_9GdTe_6 - Tl_4PbTe_3 - Tl_9BiTe_6 system based on the phase diagrams of the Tl_9GdTe_6 - Tl_4PbTe_3 and Tl_9GdTe_6 - Tl_9BiTe_6 systems using the DTA data of the ternary system.

2. Experiments and results

2.1. Boundary systems

To modeling the Tl_9GdTe_6 - $2Tl_4PbTe_3$ - Tl_9BiTe_6 ternary system, the analytical approximation of the liquidus and solidus of the boundary Tl_9GdTe_6 - $2Tl_4PbTe_3$ and Tl_9GdTe_6 - Tl_9BiTe_6 systems is necessary. The analytical approximation of the liquidus and solidus of the third boundary $2Tl_4PbTe_3$ - Tl_9BiTe_6 system was carried out in (Imamaliyeva *et al.*, 2020c). To equalize the number of atoms in the formulas of initial compounds, the thallium–lead–tellurium compound was taken as a dimer $2Tl_4PbTe_3$. To modeling of the Tl_9GdTe_6 - $2Tl_4PbTe_3$ and Tl_9GdTe_6 - Tl_9BiTe_6 systems, we used the experimental results of Babanly et al, (2008). According Babanly et al. (2008), these cross-sections are characterized by the formation of continuous solid solutions (δ -phase) with the Tl_5Te_3 structure. The Tl_9GdTe_6 - $2Tl_4PbTe_3$ and Tl_9GdTe_6 - Tl_9BiTe_6 systems are non-quasi-binary due to the incongruent melting character of the Tl_9GdTe_6 compound. As a result, in a wide compositions interval (up to 60 mol% Tl_9GdTe_6), the $TlGdTe_2$ compound first crystallizes from the melt, which leads to the formation of L+ $TlGdTe_2$ two-and L + $TlGdTe_2$ + δ three-phase areas. Below the solidus, all boundary systems are quasi-binary.

For the analytical description of the liquidus and solidus of the Tl_9GdTe_6 - $2Tl_4PbTe_3$ and Tl_9GdTe_6 - Tl_9BiTe_6 systems, the technique described in Imamaliyeva et al. (2020c; 2021) was used. The temperature dependence of the liquidus and solidus on the composition for these systems has the following forms (equations are represented in computer form).

For alloys $(1-x)(Tl_8Pb_2Te_6) - x(Tl_9GdTe_6)$:

$$T(\text{liq}) = 893.98 - 53.3 \cdot x - 40.48 \cdot x^2 \quad (1)$$

$$T(\text{sol}) = 892.6 - 138.2 \cdot x - 45.77 \cdot x^2 \quad (2)$$

$$T(\text{liq}, TlGdTe_2) = -840 + 3989 \cdot x - 1961 \cdot x^2 \quad (3)$$

For alloys $(1-x)(Tl_9BiTe_6) - x(Tl_9GdTe_6)$:

$$T(\text{liq}) = 830 - 30 \cdot x + 4.113 \cdot x^2 + 11.31 \cdot x^3 - 15.328 \cdot x^4 \quad (4)$$

$$T(\text{sol}) = 830 - 30 \cdot x - 8.16 \cdot x^2 + 7.568 \cdot x^3 + 0.54 \cdot x^4 \quad (5)$$

$$T(\text{liq}, \text{TlGdTe}_2) = 963.5 - 3210x + 7185.7x^2 - 3750x^3 \quad (6)$$

Equations (1-6) are visualized in Fig. 1:

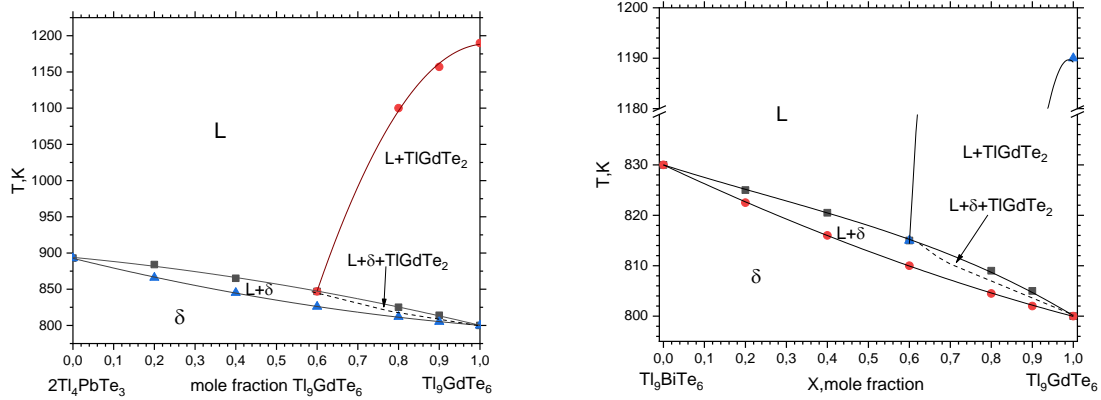


Figure 1. Phase diagram of the Tl_9GdTe_6 - $2\text{Tl}_4\text{PbTe}_3$ and Tl_9GdTe_6 - Tl_9BiTe_6 systems: symbols are results of Babanly et al. (2018), curves are visualized by equations (4-6)

2.2. Ternary system

For the 3D modeling of the liquidus and solidus surfaces of the Tl_9GdTe_6 - $2\text{Tl}_4\text{PbTe}_3$ - Tl_9BiTe_6 ternary system, the following equations are used:

$$T(\text{liq.}) = yT_{\text{liq}}(1-2) + (1-y)T_{\text{liq}}(1-3) + ay(1-y)(1-x)^2 \quad (7)$$

$$T(\text{liq}, \text{TlGdTe}_2) = yT_{\text{liq}}(1-2) + (1-y)T_{\text{liq}}(1-3) + by(1-y)(1-x)^2 \quad (8)$$

$$T(\text{solidus}) = yT_{\text{sol}}(1-2) + (1-y)T_{\text{sol}}(1-3) + T_{\text{sol}}(2-3) + cy(1-y)(1-x)^2 \quad (9)$$

Here, the compounds are designated: 1- Tl_9CdTe_6 ; 2- ($2\text{Tl}_4\text{PbTe}_3$); 3- Tl_9BiTe_6 . x -is the mole fraction of the component 1, $y = x_2 / (1-x)$; $(1-y) = x_3 / (1-x)$; x_2, x_3 -mole fraction of compounds 2 and 3. Parameters a, b, c are determined based on differential thermal analysis (DTA) data for the studied ternary system.

Inserting relations (1-6) into (7-9) we get:

$$T(\text{liq.}) = (893.98 - 53.3x - 40.48x^2)y + (830 - 30x + 4.113x + 11.31x^2 - 15.328x^3)(1-y) + 40y(1-y)(1-x) \quad (10)$$

$$T(\text{sol.}) = (892.6 - 138.2x + 45.77x^2)y + (830 - 30x - 8.16x + 7.568x^2 + 0.54x^3)(1-y) + 44y(1-y)(1-x)^2 \quad (11)$$

$$T(\text{liq., TlGdTe}_2) = (-840 + 3989x - 1961x^2)y + (963.5 - 3210x + 7185.7x^2 - 3750x^3)(1-y) \quad (12)$$

In equations (10-12) and in Fig.2: x – is mol. fractions of Tl_9GdTe_6 ; x_2 and x_3 are mol. fractions of Tl_8PbTe_3 and Tl_9BiTe_6 ; $y = x_2 / (1-x)$. In equations (11,12): $x = 0 \div 1$; $y = 0 \div 1$. In equation (12): $x = 0.65 \div 1$; $y = 0 \div 1$. Equations (10-12) are visualized in Fig. 2,3:

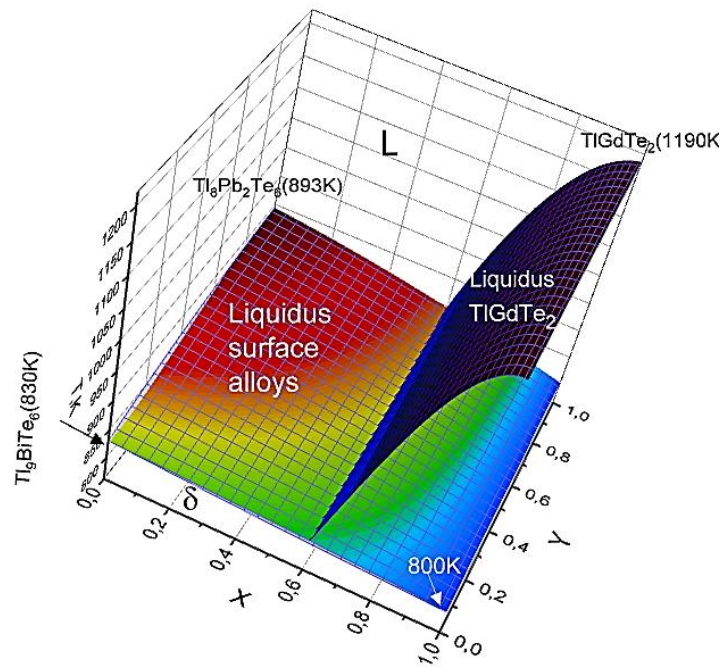


Figure 2. 3D model of the phase diagram of the Tl_9GdTe_6 - $2Tl_4PbTe_3$ - Tl_9BiTe_6 system visualized by equations (10-12)

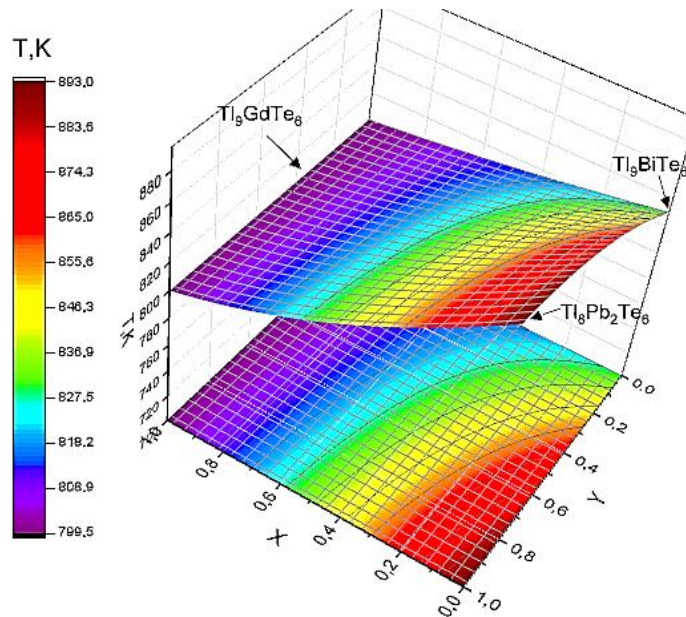


Figure 3. 3D model and projection of the solidus surface of solid solutions in the Tl_9GdTe_6 - $2Tl_4PbTe_3$ - Tl_9BiTe_6 system visualized by equation (11)

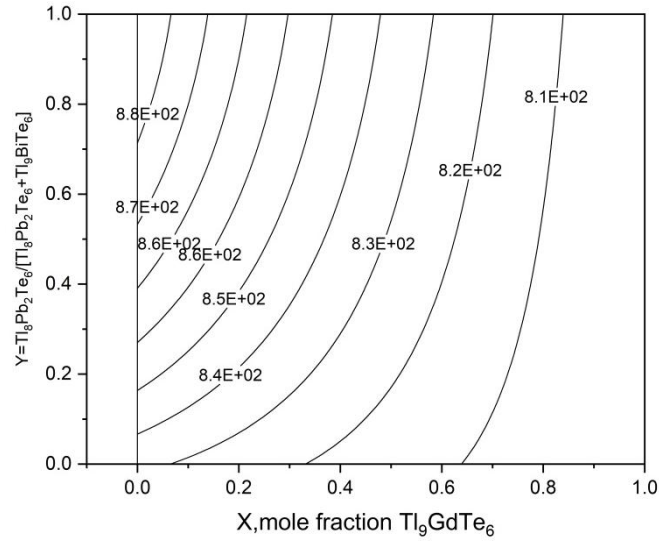


Figure 4. Temperature contours for solid solutions in the $Tl_9GdTe_6-2Tl_4PbTe_3-Tl_9BiTe_6$ system. Designation E + 02 means 10^2

2.3. Stability of solid solutions

To calculate the free energy of formation of solid solutions of the boundary systems, an asymmetric version of the model of regular solutions was used, which has been successfully tested in (Mamedov, 2015; Imamaliyeva *et al.*, 2021):

$$\Delta G_T^0 = (a + bT)x^m(1-x)^n + RT[p x \ln x + q(1-x) \ln(1-x)] \quad (13)$$

Here the first term represents the enthalpy of mixing of solid solutions in an asymmetric version of the model of regular solutions. For solid solutions with unlimited solubility, the mixing parameter is $a < 0$; $b > 0$ the second term is the configurational entropy of mixing solid solutions according to the model of non-molecular compounds (Mamedov, 2015); p and q are a number of different atoms in compounds, $R = 8.314 \text{ Jmol}^{-1} \text{ K}^{-1}$.

In equation (13) it is necessary to determine the parameter of the intermolecular interaction a and the degree of concentration m, n . For the model of strictly regular solutions, $m = n = 1$. To approximate the thermodynamic function of formation, an asymmetric version of the model of regular solutions ($m \neq n \neq 1$) should be used. To solve the equation containing two functional parameters (temperature, composition) and Gibbs excess free energy, the Multipurpose Genetic Algorithm was used (Preuss *et al.*, 2015). The following conditions were used to carry out the iteration process:

$$x=0 \div 1; a < 0; b > 0; m > n > 1; 300 \text{K} < T < 780 \text{K}$$

To determine the thermodynamic stability of solid solutions, the Lupis internal stability function (Mamedov *et al.*, 1996) was used:

$$\Psi = x(1-x) \frac{d^2(\Delta G/RT)}{dx^2} \quad (14)$$

It was found that $\Psi > 0$ in the 300-780 K temperature range in the entire range of concentrations. Hence it shows the thermodynamic stability of solid solutions in the entire interval of concentrations within 300-780 K temperature interval.

3. Conclusion

The analytical multi-3D model of the phase diagram of the $\text{Tl}_9\text{GdTe}_6\text{-Tl}_8\text{Pb}_2\text{Te}_6\text{-Tl}_9\text{BiTe}_6$ system was obtained and visualized for the quasi-ternary and nonquasi-ternary high-temperature part. For the $\text{Tl}_9\text{GdTe}_6\text{-Tl}_8\text{Pb}_2\text{Te}_6$ and $\text{Tl}_9\text{GdTe}_6\text{-Tl}_9\text{BiTe}_6$ boundary systems, the analytical models of phase diagrams of the systems were obtained in forms of temperature dependence on the composition, and their graphs are built. The thermodynamic functions of solid solutions mixing were determined using the model of regular solutions of non-molecular compounds. It was found that in the entire concentration range in the temperature range $T = 300\text{--}780$ K, the second derivative of the integral mixing free energy is greater than zero. Therefore, the values of the stability function are also greater than zero ($\Psi > 0$) in the entire range of concentrations, which indicates the thermodynamic stability of solid solutions.

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